



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification: <b>H04B 1/30, H04B 1/10</b>	<b>A1</b>	(11) International Publication Number: <b>WO 00/11794</b> (43) International Publication Date: 02 March 2000 (02.03.2000)		
(21) International Application Number: <b>PCT/EP99/06100</b> (22) International Filing Date: <b>18 August 1999 (18.08.1999)</b> (30) Priority Data: 9818397.3        25 August 1998 (25.08.1998) GB (60) Parent Application or Grant KONINKLIJKE PHILIPS ELECTRONICS N.V. [/]; (). PHILIPS PATENTVERWALTUNG GMBH [/]; (). MOORE, Paul, A. [/]; (). BARNARD, Michael, E. [/]; (). SCHWEER, Astrid [/]; (). MOODY, Colin, J.; ().	<b>Published</b>			
(54) Title: <b>LOW IF RECEIVER</b> (54) Titre: <b>RECEPTEUR FI BASSE TENSION</b>				
(57) Abstract <p>A low IF receiver suitable for use in cellular and cordless telephones and TV tuners, comprises input signal receiving means (10), quadrature related frequency down conversion means including first and second mixing means (14, 15) having first inputs (12, 13) coupled to the input signal receiving means and a local oscillator means (16) for generating a local oscillator signal having a frequency offset from a nominal centre frequency of the input signal coupled to second inputs (18, 19) of the first and second mixing means, a channel selectivity polyphase filtering means (20) for selecting a wanted channel signal from outputs of the first and second mixing means, means (26, 28, 30) for detecting when the quality of the frequency down converted signal becomes unacceptable due a large adjacent channel interfering component and means responsive to said detection for changing the local oscillator frequency by at least twice the low IF or one channel bandwidth to displace the large interfering component outside the bandwidth of the channel selectivity polyphase filtering means (20) and simultaneously changing the centre frequency of the polyphase filter.</p> <p>(57) Abrégé          La présente invention concerne un récepteur FI basse tension destiné à être utilisé dans des téléphones cellulaires sans fil et des syntoniseurs de télévision. Ce récepteur comprend un dispositif de réception de signal d'entrée (10), un dispositif de conversion de fréquence par abaissement associé à la quadrature comprenant des premier et second mélangeurs de fréquence (14, 15), présentant des premières entrées (12, 13) couplées au dispositif de réception de signal d'entrée et un oscillateur local (16) produisant un signal d'oscillation local avec un décalage de la fréquence à partir d'une fréquence centrale nominale du signal d'entrée couplé aux secondes entrées (18, 19) des premier et second mélangeurs de fréquence. En outre, ce récepteur FI basse tension comprend également un filtre polyphasé à sélectivité des trajets (20) permettant de sélectionner un signal de voie souhaitée à partir des sorties des premier et second mélangeurs, des dispositifs (26, 28, 30) permettant de détecter si la qualité du signal de conversion de fréquence par abaissement devient inacceptable en raison d'une grande composante à brouillage dans une voie adjacente, ainsi que des dispositifs qui réagissent à cette détection pour modifier la fréquence de l'oscillateur local par au moins le double de la fréquence FI basse tension ou par une bande de fréquence d'un canal pour déplacer la grande composante à brouillage à l'extérieur du filtre polyphasé à sélectivité de trajets (20) et modifier simultanément la fréquence centrale du filtre polyphasé.</p>				

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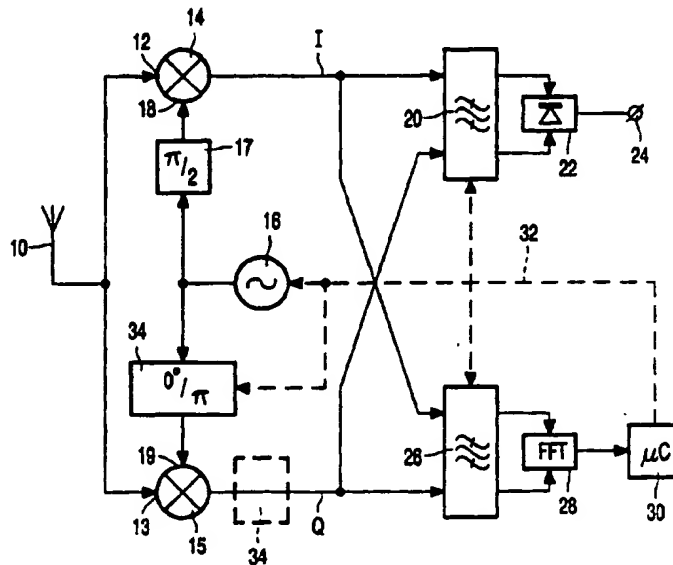
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			(43) International Publication Date: 2 March 2000 (02.03.00)
(21) International Application Number: PCT/EP99/06100		(81) Designated States: CN, JP, KR, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).	
(22) International Filing Date: 18 August 1999 (18.08.99)			
(30) Priority Data: 9818397.3 25 August 1998 (25.08.98) GB		Published With international search report.	
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(54) Title: LOW IF RECEIVER

## (57) Abstract

A low IF receiver suitable for use in cellular and cordless telephones and TV tuners, comprises input signal receiving means (10), quadrature related frequency down conversion means including first and second mixing means (14, 15) having first inputs (12, 13) coupled to the input signal receiving means and a local oscillator means (16) for generating a local oscillator signal having a frequency offset from a nominal centre frequency of the input signal coupled to second inputs (18, 19) of the first and second mixing means, a channel selectivity polyphase filtering means (20) for selecting a wanted channel signal from outputs of the first and second mixing means, means (26, 28, 30) for detecting when the quality of the frequency down converted signal becomes unacceptable due a large adjacent channel interfering component and means responsive to said detection for changing the local oscillator frequency by at least twice the low IF or one channel bandwidth to displace the large interfering component outside the bandwidth of the channel selectivity polyphase filtering means (20) and simultaneously changing the centre frequency of the polyphase filter.



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**Description**

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## DESCRIPTION

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## LOW IF RECEIVER

## 5 Technical Field

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The present invention relates to a low IF receiver, which expression is intended to cover a low IF receiver section of a transceiver. Such a receiver is suitable for fabrication as an integrated circuit for use in telecommunications products, such as cellular and cordless telephones, and TV tuners.

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## Background Art

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Low IF receivers are frequently implemented as polyphase or sequence asymmetric receivers. Figure 1 of the accompanying drawings illustrates a typical polyphase receiver. A signal received by an antenna 10 is applied to first inputs 12, 13 of quadrature related mixers 14, 15. A local oscillator 16 generating a local oscillator frequency which is offset typically by half a channel spacing from the nominal carrier frequency of the received signal is applied by way of a ninety degree phase shifter 17 to a second input of the mixer 14 and directly to a second input 19 of the mixer 15. The outputs of the mixers 14, 15 are the I and Q channels, respectively. These channels are applied to a polyphase filter 20 functioning as a band pass filter. The outputs of the polyphase filter 20 are applied to respective inputs of a demodulator 22 which provides an output, audio frequency signal on an output terminal 24.

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From Figure 1 it can be seen that the basic polyphase receiver structure is very similar to a zero IF receiver in that the IF consists of a quadrature pair of channels, the in-phase or I channel and the quadrature-phase or Q channel. However, unlike the zero-IF receiver where the local oscillator is run at the centre frequency of the wanted signal, in the polyphase case the low-IF is achieved by running the receiver local oscillator at typically half a channel spacing from the centre frequency of the wanted signal. Thus for example in GSM (Global System for Mobile Communications) with a channel spacing of 200 kHz, if the desired signal is at 950 MHz then the local oscillator could be at

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5 950.1 MHz giving an IF of 100 kHz. The principal advantage of the polyphase approach over the zero-IF approach is that large DC offsets which are unavoidably generated by the two mixers are no longer in the IF bandwidth and  
10 therefore do not interfere with the demodulation of the wanted signal.

5 From the example frequencies given it is obvious that any signal present at 950.2 MHz will form an image signal also at an IF frequency of 100 kHz. In principle this is not a problem since the polyphase filter is able to distinguish  
15 signals on its complex inputs having opposing phase relationships, as is the case between the desired and the image frequency. However, this image rejection capability is in practice limited by the level of matching and balance  
20 that can be achieved in amplitude and phase between the I and Q channels, which means that an extremely strong signal at the image frequency will cause interference to the desired signal in the IF if the desired signal is too weak. Such a problem does not appear too serious for the DECT and GSM systems  
25 because there is a relatively relaxed specification on the adjacent channel rejection required by a receiver. However if the polyphase approach is extended to other systems not having such a relaxed specification on the adjacent channel rejection then image rejection will become more of an issue.

## 20 Disclosure of Invention

35 An object of the present invention is to improve image rejection in low IF receivers.

40 According to one aspect of the present invention there is provided a low IF receiver comprising frequency down conversion means including a local oscillator, a channel selectivity polyphase filtering means for selecting a wanted  
25 channel signal from the output of the frequency down conversion means, means for detecting when the quality of the frequency down converted signal becomes unacceptable and means responsive to said detection for changing the local  
45 oscillator frequency and the centre frequency of the polyphase filter.

30 More particularly the present invention provides a low IF receiver comprising input signal receiving means, quadrature related frequency down conversion means including first and second mixing means having first inputs  
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5 coupled to the input signal receiving means and second inputs coupled to a  
local oscillator means for generating a local oscillator signal having a frequency  
offset from a nominal centre frequency of the input signal, a channel selectivity  
10 polyphase filtering means for selecting a wanted channel signal from outputs of  
the first and second mixing means, means for detecting when the quality of the  
frequency down converted signal becomes unacceptable and means  
15 responsive to said detection for changing the local oscillator frequency and the  
centre frequency of the polyphase filter.

In one embodiment of the present invention the means for changing the  
10 local oscillator frequency also inverts the sign of one of the local oscillator  
signals. The inversion of one of the local oscillator signals effectively tunes the  
polyphase filter by twice the IF.  
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In another embodiment of the present invention the detecting means  
monitors the potential image frequencies and causes the local oscillator  
25 frequency changing means to change the local oscillator frequency in response  
to deciding which image frequency to use.  
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The detecting means may comprise a wideband polyphase filter, means  
30 for identifying the frequencies present in the output of the wideband polyphase  
filter, and image frequency analysing means for providing a control signal for  
altering the frequency of the local oscillator and the centre frequency of the  
channel selectivity polyphase filtering means and the wideband polyphase filter.  
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By being able to simultaneously alter the local oscillator frequency and  
the centre frequency of channel selectivity filter and other complex signal  
processing means, such as signal de-rotation rate, it is possible to allow the  
40 image frequency to be dynamically steered away from that of any unwanted  
strong signals. This feature can be used to enhance the performance of  
inexpensive receivers so that they can meet more stringent type approval  
requirements or alternatively enable high performance products to be built which  
45 would have an on-the-air performance better than that which can be met with  
conventional superheterodyne and homodyne designs.  
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According to another aspect of the present invention there is provided an  
50 integrated circuit comprising quadrature related frequency down conversion

5 means including first and second mixing means having first inputs for an input  
signal and second inputs for a local oscillator signal having a frequency offset  
10 from a nominal centre frequency of the input signal, a channel selectivity  
polyphase filtering means for selecting a wanted channel signal from outputs of  
5 the first and second mixing means, means for detecting when the quality of the  
frequency down converted signal becomes unacceptable and means  
15 responsive to said detection for providing a control signal for changing the local  
oscillator frequency and the centre frequency of the polyphase filter.

According to a further aspect of the present invention there is provided a  
10 method of operating a low IF receiver, comprising the steps of monitoring the  
quality of a frequency down-converted signal; if the signal quality is  
20 unacceptable, changing the local oscillator frequency by the equivalent of a  
channel bandwidth; determining if the signal quality is better; and if not, reverting  
back to the prior local oscillator frequency.

#### 25 Brief Description of the Drawings

The present invention will now be described, by way of example, with  
30 reference to the accompanying drawings, wherein:

Figure 1 is a block schematic diagram of the already described zero IF  
20 polyphase receiver.

Figure 2 is a block schematic diagram of one embodiment of a low IF  
35 receiver made in accordance with the present invention,

Figure 3 shows a typical polyphase filter which can be used in the  
embodiment shown in Figure 2,

25 Figures 4A and 4B illustrate frequency distribution at RF,

Figures 5A and 5B illustrate infradyne operation,

Figures 6A and 6B illustrate supradyme operation, and

45 Figure 7 is a flow chart of an algorithm which effects a change of  
frequency conversion mode.

30 In the drawings the same reference numerals have been used to indicate  
corresponding features.



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## Modes for Carrying Out the Invention

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Compared to Figure 1, the embodiment of the invention shown in Figure 2 includes additional features, namely a wideband polyphase filter 26, Fast Fourier Transform (FFT) stage 28 and a microcontroller 30, which enable the receiver to monitor potential image frequencies and make an optimal choice at any instant of an IF and the consequent image frequency to use. One method of changing the sign of the IF in one channel, the Q channel, whilst leaving the sign of the other channel, the I channel, unchanged is to invert the phase of the local oscillator 16 output by providing a switchable inverter 34 in the local oscillator path to the input 19 of the mixer 15. An alternative method of changing the sign of the IF in one channel whilst leaving the sign of the other channel, the I channel, unchanged is to locate the inverter 34 in the output path of the mixer 15, as shown in broken lines, thus inverting the Q channel. Optionally the inverter 34 may also be used in the I channel. Digital implementations are also possible. Irrespective of the actual method of changing the sign, this always has the effect of retuning the polyphase filters 20 and 26.

More particularly the I and Q channels are coupled to the polyphase filter 26 which has a bandwidth wide enough to allow through the IF signals corresponding to potential image frequencies, which might extend for instance to three channels either side of the wanted signal. Since there is only a requirement to detect strong signals in this frequency range this filter 26 does not need a very high dynamic range, rather only enough sensitivity to guarantee detecting reliably an image signal that would cause an image rejection problem. This means that the polyphase filter 26 does not require so much resource in terms of silicon area or DSP instruction cycles as does the channel selectivity polyphase filter 20.

Figure 3 illustrates an embodiment of a 5th order polyphase filter 36 which can be used as filter 20 and/or 26 in Figure 2. The filter comprises 2 sets of stages, corresponding stages in each set being identical. For convenience of description only one set of the stages will be described and the corresponding components in the non-described set will be shown in parenthesis. A first stage

5 of the filter comprises a source resistor R1 (R3), a capacitor C1 (C6) and a  
transconductor JC1 (JC9) coupled in parallel between signal rails 38, 40. A  
10 cross-coupled gyrator consisting transconductors JC26 and JC17 is coupled to  
the signal rails 38, 40. A current source J1 (J2) representing the inputs is  
5 coupled to the signal rails 38, 40. The current sources J1, J2, correspond to  
signal inputs from the mixers 14, 15 (Figure 2).

15 The second, third and fourth stages are of identical layout and will be  
described collectively. A transconductor JC2 (JC10), JC4 (JC12), JC6 (JC14) is  
connected in parallel with a capacitance C2 (C7), C3 (C8), C4 (C9) and another  
10 transconductor JC3 (JC11), JC5 (JC13), JC7 (JC15) between signal rails 42, 44.  
20 Cross coupled gyrators JC19 (JC18), JC21 (JC20) and JC23 (JC22) are  
coupled to the signal rails 42, 44 of the respective stages. The fifth stage of the  
filter comprises a transconductor JC8 (JC16), capacitance C5 (C10) and resistor  
25 R2 (R4) connected in parallel between signal lines 46, 48. A cross coupled  
15 gyrator JC25 (JC24) is coupled to the signal rails 46, 48. Outputs are derived  
from the fifth stages. In practice the transconductors JC17 to JC26 are all  
controlled by a common current control circuit that is adjusted to tune the centre  
30 frequency of the filter 36.

Reverting to Figure 2, the signal from the wideband polyphase filter 26 is  
20 applied to the FFT stage 28 which is sufficiently refined as to identify which  
channels potential interfering signals are located in. Finally the microcontroller  
35 30 analyses the signal strengths present in all of the potential image channels  
and selects the appropriate IF frequency to minimise potential image  
breakthrough by controlling the local oscillator 16 frequency and tuning the  
40 polyphase filters 20 and 26 to the appropriate centre frequency using signals on  
25 a common control line 32.

45 If there is some latitude in the choice of IF frequency then other  
considerations, such as the lowest power setting of the receiver, may then also  
be taken into account in the final IF frequency choice.

30 The present invention is based on operating the frequency down  
conversion means, that is the mixers 14, 15 in two alternative modes, one in  
50 which the local oscillator frequency  $f_{LO}$  is greater than the nominal RF channel

5 frequency  $f_{ch}$ , so called supradyne operation and another in which  $f_{LO}$  is lower than  $f_{ch}$ , so called infradyne operation. In a simple mode of operation the microcontroller 30 switches the local oscillator frequency  $f_{LO}$  by twice the IF, that  
10 is by  $2f_{IF}$ , to identify which channels the potential interfering signals are located  
5 in.

In order to illustrate the operation of the receiver made in accordance with the present invention reference is made to Figures 4A, 4B, 5A, 5B, 6A and 6B.  
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Figures 4A and 4B show the frequency distribution at RF with the  
10 stronger interfering components being below the wanted channel  $f_{ch}$  in Figure 4A and above the wanted channel in Figure 4B. The drawings also indicate the local oscillator frequencies  $f_{LO,i}$  and  $f_{LO,s}$  and their negative counterparts for  
20 infradyne and supradyne operation.

Figures 5A and 5B show the frequency distributions at IF after  
25 quadrature conversion for infradyne operation. The bandwidth of the channel selectivity polyphase filter 20 is referenced  $B_{20}$ . The broken line indicates the practically limited rejection on the image side. By comparing Figures 5A and 5B  
30 it will be noted that in Figure 5A the larger interfering component lies within the limited image rejection of the filter 20 whereas in Figure 5B it is the smaller  
20 interfering component.

Figures 6A and 6B show the frequency distributions at IF after  
35 quadrature conversion for supradyne operation. In Figure 6A, the smaller interfering component lies within the limited bandwidth  $B_{20}$  of the filter 20 whereas in Figure 6B it is the larger component within the limited bandwidth  $B_{20}$   
40 of the filter.  
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By making the bandwidth of the wideband polyphase filter 26 equal to at least 3 channel bandwidths it is possible to determine where a larger interfering component lies and to eliminate it by simply selecting a local oscillator frequency  
45  $f_{LO}$  to give infradyne or supradyne operation, and changing the centre frequency  
30 of the filter 26 accordingly.

Figure 7 is a flow chart of an algorithm which effects a change of frequency conversion mode in the case of poor quality reception.  
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Block 50 denotes monitoring signal quality by comparing the signal with a threshold value, for example by considering the bit error rate in a repeatable signal such as a training sequence and/or synchronisation code word, averaged over a predetermined number of bursts or repeats. In block 52 a check is made to see if the measured quality is unacceptable. If the answer is No (N) then the flow chart reverts to the block 50. However if the answer is Yes (Y), then in block 54 the local oscillator frequency is changed by the equivalent of one channel bandwidth, for example 200kHz in the case of GSM. In block 56 a figure of merit is determined and in block 58 a check is made to see if the reception is better. If the answer is Yes (Y) the flow chart reverts to the block 50. If the answer is No (N), in block 60 the local oscillator frequency is changed back to its original value and the flow chart reverts to the block 50.

In operation the figure of merit of reception should be verified periodically because accumulating changes in operation may lead to the threshold being too small. Using the quality of the previously received signal, the threshold could be increased for a predetermined period.

In situations of failing reception leading to the loss of a call-in-progress and a failed connection, the mode of frequency conversion should be changed.

In the event of finding big interferers before and after shifting the IF by twice the IF frequency and the microcontroller 30 not being able to decide on the better IF, it can as a final option operate the receiver as a zero IF receiver by shifting the IF by one IF and altering the polyphase filter characteristic so that it appears effectively as 2 filters. This may be done by adjusting the cross coupling, that is, between transconductors JC17 and JC26; JC18 and JC19, JC20 and JC21, JC22 and JC23, and JC24 and JC25 so that the currents are zero.

In the present specification and claims the word "a" or "an" preceding an element does not exclude the presence of a plurality of such elements. Further, the word "comprising" does not exclude the presence of other elements or steps than those listed.

From reading the present disclosure, other modifications will be apparent to persons skilled in the art. Such modifications may involve other features

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which are already known in the design, manufacture and use of low IF receivers and component parts thereof and which may be used instead of or in addition to features already described herein.

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#### 5 Industrial Applicability

Low IF radio receivers and integrated circuits comprising such receivers.

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## Claims

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## CLAIMS

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1. A low IF receiver comprising frequency down conversion means including a local oscillator, a channel selectivity polyphase filtering means for selecting a wanted channel signal from the output of the frequency down conversion means, means for detecting when the quality of the frequency down converted signal becomes unacceptable and means responsive to said detection for changing the local oscillator frequency and the centre frequency of the polyphase filter.

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2. A low IF receiver comprising input signal receiving means, quadrature related frequency down conversion means including first and second mixing means having first inputs coupled to the input signal receiving means and second inputs coupled to a local oscillator means for generating a local oscillator signal having a frequency offset from a nominal centre frequency of the input signal, a channel selectivity polyphase filtering means for selecting a wanted channel signal from outputs of the first and second mixing means, means for detecting when the quality of the frequency down converted signal becomes unacceptable and means responsive to said detection for changing the local oscillator frequency and the centre frequency of the polyphase filter.

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3. A receiver as claimed in claim 2, characterised in that said means changes the local oscillator frequency by at least twice the low IF.

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4. A receiver as claimed in claim 3, characterised in that the means for changing the local oscillator frequency also inverts the sign of the local oscillator signal.

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5. A receiver as claimed in claim 3, characterised in that said means in response to finding that an unacceptable signal is present at both the respective local oscillator frequencies, adapts the polyphase filtering means to operate as two zero IF filters.

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6. A receiver as claimed in claim 2, characterised in that the detecting means monitors image frequencies and causes the local oscillator frequency changing means to change the local oscillator frequency in response to deciding which image frequency to use.

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7. A receiver as claimed in claim 1, characterised in that the detecting means comprises a wideband polyphase filter, means for identifying the frequencies present in the output of the wideband polyphase filter, and image frequency analysing means for providing a control signal for altering the frequency of the local oscillator and the centre frequency of the channel selectivity polyphase filtering means and the wideband polyphase filter.

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8. A receiver as claimed in claim 2, characterised in that the detecting means comprises a wideband polyphase filter, means for identifying the frequencies present in the output of the wideband polyphase filter, and image frequency analysing means for providing a control signal for altering the frequency of the local oscillator and the centre frequency of the channel selectivity polyphase filtering means and the wideband polyphase filter.

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9. An integrated circuit comprising quadrature related frequency down conversion means including first and second mixing means having first inputs for an input signal and second inputs for a local oscillator signal having a frequency offset from a nominal centre frequency of the input signal, a channel selectivity polyphase filtering means for selecting a wanted channel signal from outputs of the first and second mixing means, means for detecting when the quality of the frequency down converted signal becomes unacceptable and means responsive to said detection for providing a control signal for changing the local oscillator frequency and the centre frequency of the polyphase filter.

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10. A method of operating a low IF receiver, comprising the steps of:  
monitoring the quality of a frequency down-converted signal;

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if the signal quality is unacceptable, changing the local oscillator frequency by the equivalent of a channel bandwidth;

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determining if the signal quality is better; and

if not, reverting back to the prior local oscillator frequency.

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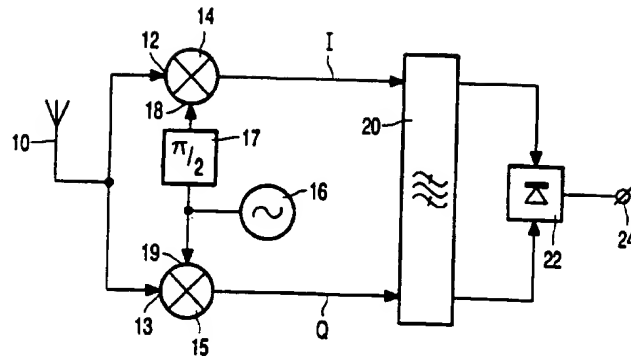


FIG. 1

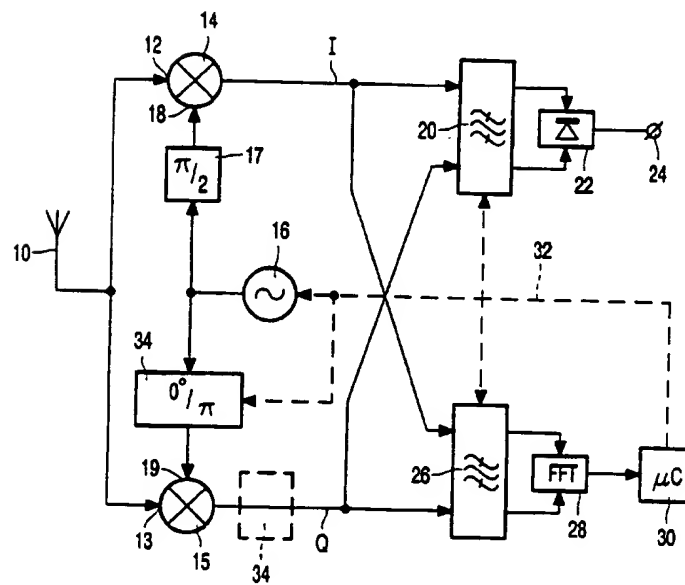


FIG. 2

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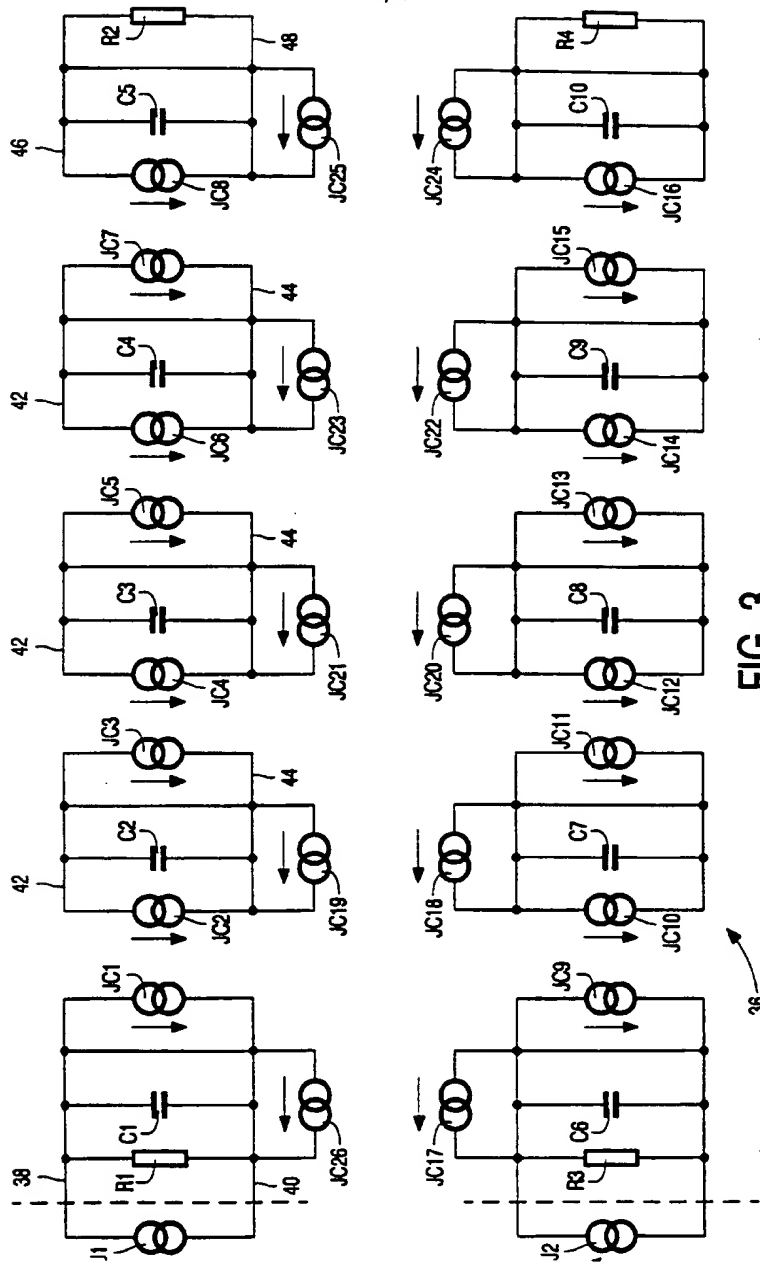


FIG. 3

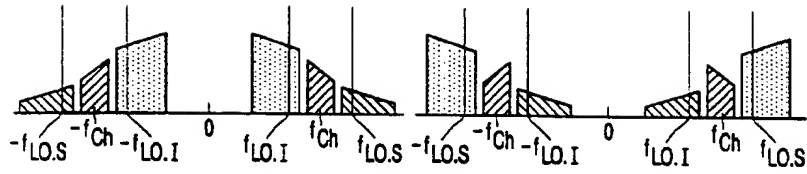


FIG. 4A

FIG. 4B

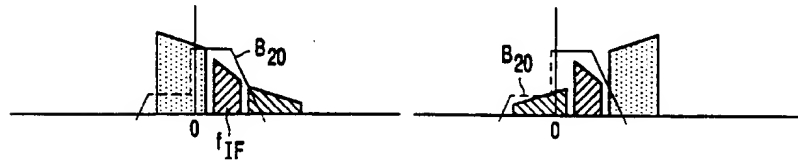


FIG. 5A

FIG. 5B

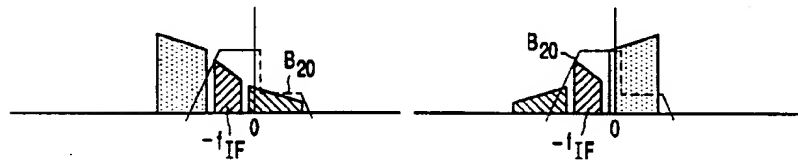


FIG. 6A

FIG. 6B

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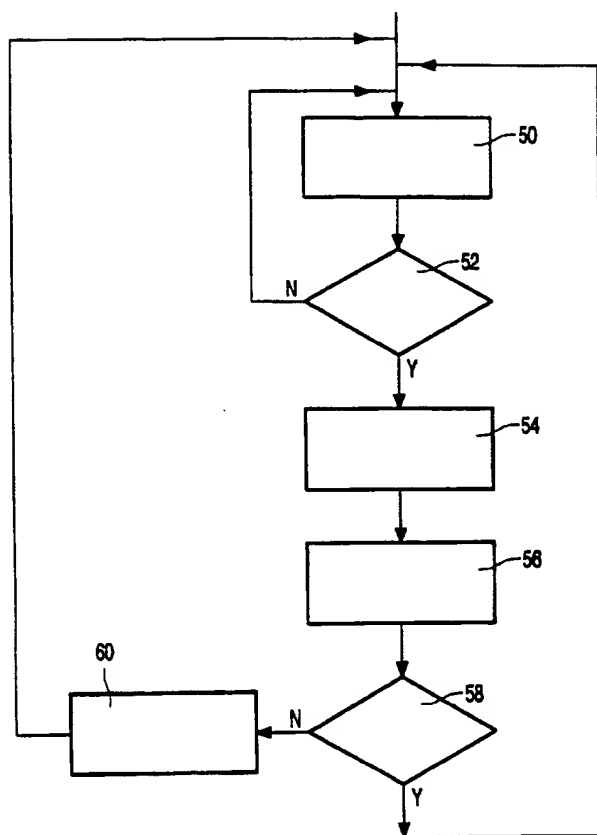


FIG. 7

# INTERNATIONAL SEARCH REPORT

International Application No.  
PCT/EP 99/06100

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 7 H04B1/30 H04B1/10

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 H04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	DE 43 03 903 A (HEINZMANN GUSTAV DR ING) 24 February 1994 (1994-02-24) abstract; figures 1-4	1-10
A	EP 0 797 292 A (PHILIPS ELECTRONICS NV) 24 September 1997 (1997-09-24) column 3, line 27 -column 5, line 6; figure 3	1-10
A	EP 0 542 520 A (NOKIA MOBILE PHONES LTD) 19 May 1993 (1993-05-19) column 2, line 34 -column 3, line 17; figures 3,4	1-4,9,10

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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- "Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
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Date of the actual completion of the international search

17 November 1999

Date of mailing of the international search report

25/11/1999

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# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No  
PCT/EP 99/06100

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
DE 4303903 A	24-02-1994	NONE	
EP 0797292 A	24-09-1997	CN 1164782 A JP 10070482 A	12-11-1997 10-03-1998
EP 0542520 A	19-05-1993	FI 915388 A DE 69218551 D DE 69218551 T US 5396657 A	15-05-1993 30-04-1997 11-09-1997 07-03-1995

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